

**ANALYSIS OF DYNAMIC STRESS PROPAGATION OF A VIBRATING SUBSEA
STRUCTURE IN A PRESSURIZED ENVIRONMENT**

by

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**SCHOOL OF POST-GRADUATE STUDIES
UNIVERSITY OF LAGOS, AKOKA, LAGOS
*CERTIFICATION***

This is to certify that the thesis

**“ANALYSIS OF DYNAMIC STRESS PROPAGATION OF A VIBRATING SUBSEA
STRUCTURE IN A PRESSURIZED ENVIRONMENT”**

Submitted to the School of Post-Graduate Studies University of Lagos for the award of the
degree of

DOCTOR OF PHILOSOPHY

is a record of original research carried out by

OGUNMOLA, Ogunbayo Yemisi

in the Department of Mechanical Engineering

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DEDICATION

in

Loving Memory of my Late Father
(Pa Joseph Ogunmola Oguntobi)

and to my

Mother, Wife, Siblings and Teachers

and to

The Almighty God

ABSTRACT

Offshore pipeline and flow line systems define a variety of subsea architectures associated with Floating Production Storage and Offloading units (FPSOs) or Floating Storage and Offloading units (FSOs) that are usually employed for oil and gas production in deep and ultra deep waters. The design of such transmission facilities, must satisfactorily account for various phenomena such as hydrodynamic wave loading, fluid transport velocity, operating pressure and temperature of the internal fluid as well as limitations imposed by the seabed subsoil layer geotechnical properties. In fact the transverse and longitudinal dynamic responses of these pipeline and flow line systems are strongly modulated by these effects. Subsea pipelines are on the high demand to function at high temperatures and pressures. The natural behavior of a pipeline is to relieve the attendant high axial stress in the pipe-wall by buckling. Such uncontrolled buckling can have serious implication on the integrity of a pipeline. Hence, the usual practice to date, in the industry is to restrain pipelines by trenching and burying, or relieving the stress with inline expansion spools. In this work, the effect of transverse and longitudinal vibrations on the dynamic stresses induced by the fluid flow was studied with special reference to onset of buckling or bursting of such pipes. For this purpose, an offshore pipeline was idealized as a fluid conveying elastic beam on an elastic foundation and the corresponding set of equations governing the transverse and longitudinal motion of the pipe were formulated. Particularly, by employing integral transforms, an analytic solution for the induced stresses was computed and simulated for design applications while comparison with corresponding formulae currently in use in the field was also carried out. Furthermore, the earlier work was extended to capture the effect of deliberate or natural sediment covering of pipe that occurs over a long period of time, by examining the dynamic stress propagation through a partially or fully buried offshore pipeline. For this problem a boundary valued partial differential equation for the fluid- structure- soil interaction mechanics was formulated. In particular, by employing operational methods, the burst and buckling pressure profiles as modulated by the seabed sediment layer history were reported for design analysis and applications. Lastly this research reported an analytic solution for the induced stresses in polar coordinates coupled with von Mises yield criterion in conjunction with the corresponding set of equations governing the transverse and longitudinal motions of an offshore pipeline on an elastic foundation. Interesting results were simulated for practical analysis and applications.

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NOTATION

A	pipe cross sectional area after deformation
A_o	original cross sectional area of pipe
A_p	surface area of pipe
A'	change in the surface area of the pipe
C_1	damping force per unit velocity in the transverse direction
C_2	damping force per unit velocity in the axial direction
C_D	hydrodynamic drag coefficient
E	Young modulus of elasticity
$F_1(t)$	external force in the transverse direction
$F_2(t)$	external force in the longitudinal direction
g	acceleration due to gravity
h	depth of pipe below sea level
I	moment of inertia
k_b	stiffness of the sea bed
L	length of pipe
m	sum of the masses of pipe and fluid
m_f	mass of flowing fluid in side the pipe
m_w	mass of sea water displaced by pipe
M	sum of masses of pipe, fluid in pipe and external water displaced by pipe

p_A	pressurization effect
P_h	hydrodynamic effect of the ocean
p_o	pressure at entry
T_o	tension in pipe
t	time
u	longitudinal displacement
U	velocity of fluid flowing inside pipe
U'	differential of velocity with respect to x
\dot{U}	differential of fluid velocity with respect to time
\tilde{u}	longitudinal response in Laplace plane
u^F	longitudinal response in Fourier plane
\tilde{u}^F	longitudinal response in Fourier-Laplace plane
w	transverse displacement
\tilde{w}	transverse response in Laplace plane
w^F	transverse response in Fourier plane
\tilde{w}^F	transverse response in Fourier-Laplace plane
x	axial displacement coordinate
z	transverse displacement coordinate
r_i	internal radius of pipe
r_o	external radius of pipe

B_r = the body force in the r direction

\bar{a}_r = the acceleration in the r direction

Greek letters

α coefficient of thermal expansivity

γ coefficient of area deformation

$\Delta\Theta$ temperature change from inlet to outlet

Δp pressure change from inlet to outlet

Θ temperature of the flowing fluid

Θ' temperature gradient

μ coefficient of sliding friction

∇^2 Laplacian operator

∇ gradient operator

ρ_w density of water

Φ velocity potential

σ_y transverse bending stress

σ_x axial bending stress

σ_r radial bending stress

σ_θ Hoop stress

$\tau_{\theta r}, \tau_{r\theta}$ radial shear stresses

$\tau_{(xz)1}$, shear stress on the upper layer

$\tau_{(xz)2}$, shear stress on the lower layer

δ_s sediment layer